PHYSIK INSTRUMENTE

Electromagnetic levitation for atomic resolution positioning

Rudolf Krüger Technology Center Magnetic Drives & Systems Dresden 16.11.2023



 \mathbf{PI}

Motivation Looking back at 2022...



15. Tagung 'Feinwerktechnische Konstruktion' 2022 | Dr. Christian Rudolf | © PI 2022





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External

Why magnetic levitation (MagLev)?

Eliminating the restrictions of mechanical guiding elements and couplings

- Full control in six degrees of freedom
- Completely frictionless guiding no rolling elements, no lubrication, no air flow
- No stick-slip effects
- No abrasion or wear, no particle generation
- Vacuum compatibility

MagLev technology has the potential to achieve ultra-high precision in dynamic and continuous (maintenance free) operation!

Magnetic levitation at PI



PIMag6D

- Planar stage with six actuation coils
- 100 mm x 100 mm x 0,1 mm
- Up to 100 mm/s
- Resolution < 10 nm



Mag6D

- Planar stage with 144 PCBintegrated coils
- Decentralized drive and sensor modules
- 120 mm x 120 mm x 1.6 mm

MagLin 6D

- Linear stage with 6 DoF micropositioning capability
- Integrated electronics
- Powerless levitation
- 45 mm x 0.5 mm x 0.5 mm
- Resolution < 5 nm</p>



Background and motivation for the new development **Project overview for MetExSPM**

Metrological Express Scanning Probe Microscope













The task at hand...

... and specification requirements

Planar motion stage for sample positioning and scanning Motion range

- Motion range in XY plane = 12.7 mm x 12.7 mm
- Motion in Z = ±0.25 mm
- Rotary motion (roll, pitch and yaw) = ±0.25°

Dynamics

- Motion velocity (XY plane) = 10 mm/s
- Acceleration (XY plane) = 1 m/s²
- Bandwidth (1 μ m amplitude) \approx 100 Hz

Precision

Position resolution < 0.1 nm





The task at hand... ... and key challenges

Sensor system

- Sub-nanometer resolution sensors for 6 DoF measurements
- Precision and accuracy with respect to planar travel range
- Robustness against distance changes and rotation

Thermal effects and long-term stability

- Management of losses from active components (actuators and sensors)
- Powerless levitation
- Separation of force and metrology loops
- Ultra-low expansion materials (integration and interface design)





Architecture of the MagLev stage

- Decoupled force and metrology loops
- Metrology frame made from ultra-low expansion material
- Integrated mirrors for reference metrology
- Thermo-mechanical decoupling for mover frames



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Actuator configuration

4x Bearing actuators for (near) powerless levitation (Z, rotX, rotY)

- Reluctance force actuators with integrated gravity compensation (for a mover mass of 1 kg plus a load of 100 g)
- Consistent points of force actuation on the mover
- Force constant k_i = 2.45 N/A
- Motor constant $k_M = 2.21 \text{ N/VW}$

4x Linear motors for long-stroke planar motion (X, Y, rotZ)

- Over-sized Lorentz force actuators for minimized losses
- Optimized for minimum cross-talk with Z-actuators
- Force constant k_i = 1.11 N/A
- Motor constant $k_M = 1.52 \text{ N/VW}$



*Lighter components (active) fixed to frame, darker components (passive) fixed to mover!



Thermal performance of XY-motors

Simulation of exemplary step-settle-motion for raster scanning application

- Maximum jerk determines step time for equal step size
- Step size: 1 μm and 100 nm
- Three different jerk values: 0.1 m/s³, 1 m/s³ and 10 m/s³

Findings

- The average power demand during a step is < 20 μW
- Considering the settling and measurement times, average power during a scan motion is even smaller
- Note that time values on the right only include step times and not the respective settling times





Metrology concept

- Optical encoders for XY-motion and rotation about Z
- Interferometers for Z-motion and tip-tilt (rotation about X and Y)
- Sensor redundancy for improved signal-to-noise ratio per DoF
- Completely passive mover with integrated mirror surfaces and custom linear gratings for planar motion







Encoder for X, Y and yaw (rotZ) Resolution and noise (at 64,000 interpolation and f_s = 10 kHz)





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Encoder for X, Y and yaw (rotZ) Exemplary position measurement

- Raw sine-cosine-signals into interpolator, counts per SPI into C-702 controller (sample rate f_s = 10 kHz, no additional filters or data processing)
- P-752 piezo stage in open-loop mode (voltage ramp with 7 mV at 10 Hz)







Encoder for X, Y and yaw (rotZ)

Robustness against distance changes and angular misalignment

Sine and cosine levels of the 1 V_{pp} signal for single axis misalignment







Encoder for X, Y and yaw (rotZ) Robustness against distance changes and angular misalignment

Sine levels of the 1 V_{pp} signal for multi-axis misalignment







Encoder for X, Y and yaw (rotZ) Robustness against distance changes and angular misalignment

Resulting phase errors for multi-axis misalignment





Integration aspects of ultra-low expansion materials General issues

Different CTEs of glass and metal components

... in combination with brittle properties of glass and glass-ceramics

Why is this relevant?

- Thermal effects cannot be neglected! Sensors and actuators will generate a certain amount of heat!
- Active cooling would introduce additional disturbances (vibrations)

Critical mechanisms for equivalent stress in glass-ceramic components

- Expansion of metal inserts (and adhesives)
- Bolt pretension
- Expansion of the actuator frame



Metal inserts in ultra-low expansion glass-ceramic **Insert and interface design for actuator frame interface**

- Insert made from Invar (D = 6.3 mm with M3 thread)
- Epoxy-based adhesive (curing at room temperature with minimal shrinkage)
- Radial alignment via seal rings (acting as additional adhesive barriers)
- Protruding installation in glass-ceramic to allow bolt pretension







Thermo-mechanical decoupling of actuator and metrology frames General issues and solution approach for integration of brittle ultra-low expansion materials

Conflicting objectives result in compromise

- Minimal amount of thermally induced stress in glass-ceramic \rightarrow compliant coupling between actuator and metrology frames
- Dynamically precise actuation of the mover → stiff coupling between actuator and metrology frames

Solution approach

 Flexure-based decoupling mechanism allowing for deformation of the actuator frame (in the XY-plane) while maintaining a sufficiently stiff connection between actuator and metrology frame









Thermo-mechanical decoupling of actuator and metrology frames Simulation-based proof of concept

Simulation setup

- Flexures modelled via 6-DoF bushings with stiffness matrix
- Inserts and adhesives fully modelled
- Bolt pretension included in initial load step
- Evaluation of deformation and equivalent stress in glass-ceramic component for extended temperature range (±10 K)





Thermo-mechanical decoupling of actuator and metrology frames Simulation-based proof of concept

Findings (exemplary data for temperature +10 K)

- Force reaction significantly reduced from 130 N to < 4 N per insert
- Deformation of glass-ceramic reduced from 2 μm to < 40 nm
- Stress in glass-ceramic component reduced from 11 MPa to < 7 MPa note that this value corresponds to a base level due to
 expansion of insert, contribution of actuator frame deformation account to less than 1 MPa







Thermo-mechanical decoupling of actuator and metrology frames Impact on eigenmodes and frequencies of the mover





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